PRINT DATE: 08/25/95

FAILURE MODES EFFECTS ANALYSIS (FMEA) — CRITICAL HARDWARE

NUMBER: MS-1MR-BM010-X

BUBSYSTEM NAME: MECHANICAL - EDS

REVISION:

9/1/95

PART NAME YENDOR NAME

PART NUMBER VENDOR NUMBER

LRU

: DOCKING MECHANISM ASSEMBLY

33U.6316.003-05

SRU

NPO-ENERGIA : ASSEMBLY, DIFFERENTIAL

33U.6316.003-05 33U.6321.004

NPO-ENERGIA

33U.6321.004

### PART DATA

EXTENDED DESCRIPTION OF PART UNDER ANALYSIS: DIFFERENTIAL ASSEMBLY

REFERENCE DESIGNATORS:

QUANTITY OF LIKE ITEMS: 1

ONE

#### FUNCTION:

THE DIFFERENTIAL ASSEMBLY IS THE PRIMARY COMPONENT IN THE KINEMATIC CHAIN AND PERFORMS THE FOLLOWING FUNCTIONS: (1) ENSURES DEPENDENT MOVEMENT OF EACH BALLMUT PAIR; (2) LOCKS BALLMUT PAIRS TO LIMIT THEIR MOVEMENT RELATIVE TO EACH OTHER (FIXATOR); (3) ENABLES EXTENSION AND RETRACTION OF THE DOCKING RING BY THE EXTEND/RETRACT ACTUATOR: (4) PROVIDES FORCED SUMMED INPUTS TO THE FRICTIONAL BRAKE; AND (5) PROVIDES CENTERING OF RING IN PITCH AND YAW DIRECTIONS (SPRING MECHANISMS). CONTAINED IN THE DIFFERENTIAL ASSEMBLY ARE THE "RING INITIAL POSITION" SENSOR AND 'RING FORWARD POSITION' SENSOR. EACH IS DESCRIBED BELOW:

RING INITIAL POSITION SENSOR - ONCE THE DOCKING RING REACHES IT'S INITIAL POSITION, ABOUT 335 MM FROM ITS FULLY RETRACTED POSITION, A SENSOR DRIVEN FROM THE FINAL SUMMING GEAR STAGE OF THE DIFFERENTIAL ASSEMBLY SENOS REDUNDANT SIGNALS TO THE DSCU. THESE SIGNALS ARE USED TO AUTOMATICALLY TURN OFF THE EXTEND/RETRACT ACTUATOR AT THE POINT WHERE INITIAL POSITION OF THE FING IS ACHIEVED AND IS USED TO ILLUMINATE THE "RING INITIAL POSITION" INDICATOR LIGHT ON THE DOCKING CONTROL PANEL. RING INITIAL POSITION IS ALSO DOWNLINKED FOR GROUND CREW MONITORING.

RING FORWARD POSITION SENSOR - A SECOND SENSOR DRIVEN FROM THE FINAL SUMMING GEAR STAGE OF THE DIFFERENTIAL ASSEMBLY SENSES WHEN THE DOCKING RING IS FULLY EXTENDED AND SENDS REDUNDANT SIGNALS TO THE DSCU TO TURN OFF THE EXTEND/RETRACT ACTUATOR, CONTINUE AUTOMATIC DOCKING SEQUENCE (RETRACT RING), AND TO ILLUMINATE THE "RING FORWARD POSITION" INDICATOR LIGHT ON THE DOCKING CONTROL PANEL. RING FORWARD POSITION IS DOWNLINKED FOR GROUND MONITORING.



PAGE: 162 PRINT DATE: 08/25/96

FAILURE MODES EFFECTS ANALYSIS (FMEA) -- CRITICAL HARDWARE NUMBER: MI-1 MR-8M010-X

SERVICE IN BETWEEN PLIGHT AND MAINTENANCE CONTROL: VISUAL INSPECTION, SERVICEABILITY CONTOL, DOCKING WITH CALIBRATING DOCKING MECHANISM.

MAINTAINABILITY
REPAIR METHOD - NONE (REPAIRING IN MANUFACTURING CONDITIONS ONLY).

REFERENCE DOCUMENTS: 33U.6321.004 33U.6316.003-05

PRINT DATE: 06/25/95

FAILLIRE MODES EFFECTS ANALYSIS (FMEA) - CIL FAILURE MODE

NUMBER: M6-1MR-8M016-01

REVISION#

9/1/95

SUBSYSTEM NAME: MECHANICAL - EDS LRU: DOCKING MECHANISM ASSEMBLY ITEM NAME: ASSEMBLY, DIFFERENTIAL

CRITICALITY OF THIS FAILURE MODE: 2/2

FAILURE MODE:

JAMMING, INCREASED RESISTANCE

MISSION PHASE:

00

ON-ORBIT

VEHICLE/PAYLOAD/KIT EFFECTIVITY: 104 ATLANTIS

CAUSE:

CONTAMINATION, STRUCTURAL FAILURE DUE TO MECHANICAL/THERMAL SHOCK OR MANUFACTURE/MATERIAL DEFECT

CRITICALITY 1/1 DURING INTACT ABORT ONLY? NO

CRITICALITY 1R2 DURING INTACT ABORT ONLY (AVIONICS ONLY)? N/A

REDUNDANCY SCREEN

A) NA

B) N/A

C) N/A

PASS/FAIL RATIONALE:

A)

N/A

B)

N/A

C) N/A

METHOD OF FAULT DETECTION:

A JAMMED DIFFERENTIAL CAN BE DETECTED THROUGH VISUAL OBSERVATION FOLLOWING CAPTURE. LOSS OF RING EXTENSIONALIGNMENT/CAPTURE/ RETRACTION CAN BE DETECTED BY THE AFFECTED INDICATIONS ON THE DOCKING CONTROL PANEL THIS INFORMATION IS ALSO PROVIDED FOR GROUND MONITORING OF THE DOCKING PROCESS.

### - FAILURE EFFECTS -

(A) SUBSYSTEM:

PREVENTS MOVEMENT OF ALL ELEMENTS IN THE KINEMATIC CHAIN. AN INCREASED MOMENT OF RESISTANCE COULD BE OVERCOME BY THE POWER OF THE DOCKING MECHANISM ASSEMBLY ALLOWING THE RING TO BE EXTENDED, ALIGNED, OR RETRACTED. HOWEVER, TOTAL JAMMING OF THE DIFFERENTIAL WOULD PRECLUDE



PAGE: 164 PRINT DATE: 08/25/95

FAILURE MODES EFFECTS ANALYSIS (FMEA) - CIL FAILURE MODE

NUMBER: MO-1MR-BM010-01

RING EXTENSION, ALIGNMENT, CAPTURE, OR RETRACTION DEPENDING ON WHEN FAILURE OCCURS.

(B) INTERFACING SUBSYSTEM(\$):
EXCESSIVE LOADS INCURRED DURING DOCKING AS THE RESULT OF A JAMMED
DIFFERENTIAL ASSEMBLY COULD PROPAGATE TO EXTERNAL AIRLOCK AND ORBITER
STRUCTURE.

(C) MISSION:

AT THE STAGE OF DOCKING, EXTERNAL FORCES COULD OVERCOME AN INCREASED MOMENT OF RESISTANCE IN WHICH CASE DOCKING CAN BE COMPLETED. HOWEVER, IN THE EVENT OF COMPLETE JAMMING, DOCKING WOULD BE IMPOSSIBLE. EXCESSIVE LOADS INCURRED DURING CONTACT COULD CAUSE DAMAGE TO ORBITER AND MIR DOCKING MECHANISMS RESULTING IN THE INABILITY TO EXTEND OR RETRACT DOCKING RING. THE INABILITY TO MOVE RING TO MATE BOTH MECHANISMS WILL RESULT IN LOSS OF DOCKING AND SUBSEQUENT LOSS OF ORBITER/MIR MISSION OBJECTIVES.

(D) CREW, VEHICLE, AND ELEMENT(S): EXCESSIVE LOADS EXPERIENCED AS THE RESULT OF A JAMMED DIFFERENTIAL COULD RESULT IN DAMAGE TO ORBITER AND MIR DOCKING MECHANISMS. CREW AND ORBITER STRUCTURE ARE UNAFFECTED BY THESE LOADS.

(E) FUNCTIONAL CRITICALITY EFFECTS: N/A

DESIGN CRITICALITY (PRIOR TO OPERATIONAL DOWNGRADE, DESCRIBED IN F): 2/2

(F) RATIONALE FOR CRITICALITY CATEGORY DOWNGRADE:
N/A (THERE ARE NO WORKAROUNDS TO CIRCUMVENT THIS FAILURE.)

### -DISPOSITION RATIONALE-

(A) DESIGN:
DESIGN OF THE DIFFERENTIAL PROVIDES SUFFICIENT FREEPLAY BETWEEN SURFACES
TO ALLOW FOR TEMPERATURE EXPANSION AND TO PREVENT JAMMING. SPRING.
MECHANISMS ARE USED TO REDUCE SPACING BETWEEN GEARS TO PREVENT TEETH
BREAKAGE DURING PERIODS OF HIGH LOADS. WHERE APPROPRIATE GRAPHITE
LUBRICATION IS PROVIDED TO PREVENT SURFACES FROM STICKING. DIFFERENTIAL IS

ENCLOSED TO REDUCE CONTAMINATION POTENTIAL. JAMMING CAN BE COUNTERACTED BY STRENGTH OF STRUCTURAL PARTS WHICH HAVE A SAFETY MARGIN NO LESS THAN 1.4.

LOAD ANALYSIS HAS SHOWN THAT THE MAXIMUM AXIAL TENSION LOAD INCURRED AS THE RESULT OF A JAMMED DIFFERENTIAL PRIOR TO CAPTURE IS 3281 KGF ALONG THE Z-AXIS WHICH IS NOT HIGH ENOUGH TO CAUSE A CAPTURE LATCH TO DISENGAGE.

(ANALYSIS HAS SHOWN THAT AN AXIAL LOAD OF 3698 KGF IS REQUIRED TO DISENGAGE A CAPTURE LATCH.) STRESS ANALYSIS HAS INDICATED THAT THE CAPTURE LATCH WILL NOT BE DAMAGED IN SUCH A WAY AS TO TO PREVENT IT FROM BEING ACTUATED OPEN DUE TO THIS 3281 KGF AXIAL TENSION LOAD. THIS AXIAL LOAD WILL NOT EXCEED EXTERNAL AIRLOCK (ORBITCH STRUCTURAL LIMITS.



PRINT DATE: 08/25/95

FAILURE MODES EFFECTS ANALYSIS (FMEA) - CIL FAILURE MODE

NUMBER: M8-1MR-BM010-- 01

(B) TEST:

DOCKING MECHANISM ACCEPTANCE TESTS:

- 1. INSPECTION SERVICEABILITY TEST DURING THE GUIDE RING FUNCTIONAL PERFORMANCE TEST THE DOCKING MECHANISM RING IS EXTENDED TO IT'S INITIAL POSITION AND THEN IT'S FORWARD POSITION AND THEN RETRACTED TO IT'S FINAL POSITION. DIFFERENTIAL IS VERIFIED FOR PROPER OPERATION DURING RING EXTENSION AND RETRACTION.
- 2. VIBRORESISTENT TEST APOS SUBJECTED TO THE FOLLOWING VIBRATION LEVELS FOR 2 MINUTES PER AXIS:

FREQUENCY (HZ)	SPECTORAL DENSITY ACCELERATION
FROM 20 TO 80	INCREASING, 3DB OCTAVE TO 0.04G2/HZ
FROM 80 TO 350	PERMANENT 0.04G <sup>2</sup> /HZ
FROM 350 TO 2000	DECREASING 3DB OCTAVE WITH 0.04G <sup>2</sup> /HZ

SUBSEQUENT TO THIS TEST AN ENGINEERING INSPECTION IS PERFORMED TO IDENTIFY BROKEN OR LOOSE HARDWARE AND A FUNCTIONAL CHECK IS PERFORMED, PER ATP #1 ABOVE, TO VERIFY PROPER OPERATION OF THE DIFFERENTIAL

- 3. DOCKING MECHANISM CHECKOUT (STATIC) TEST RING IS EXTENDED AND RETRACTED AS NECESSARY TO FULLY TEST ITS OPERATION DURING A SINGLE DOCKING. FORCE IS APPLIED TO THE RING TO SIMULATE LOADS THAT CAN OCCUR DURING RING CAPTURE AND MATING OF THE TWO MECHANISMS. ATTENUATION SYSTEM CHARACTERISTICS IS DETERMINED WHEN THE RING IS DEFLECTED AND ROTATED DURING THIS TEST. A CHECK OF RING RETRACTION FORCE AND FORCE GENERATED AND KEPT BY THE DOCKING MECHANISM IS PERFORMED. THIS TEST WILL VERIFY PROPER OPERATION OF THE DIFFERENTIAL UNDER LOAD AND NO-LOAD CONDITIONS.
- 4. THERMO VACUUM TEST DOCKING OF THE MECHANISM IS THERMALLY CYCLED, UNDER LOAD CONDITIONS, FROM +20°C TO -50'-55°C TO +50'+55°C TO +20°C IN A VACUUM AT 10°4 TO 10°8 TORR. DWELL AT EACH TEMPERATURE AND BETWEEN OPERATIONS AT EACH TEMPERATURE IS A MINIMUM OF 60 MINUTES AFTER STABILIZATION. OPERATIONS INCLUDES PERFORMING DOCKING WHICH IS ACCOMPLISHED AT A SPEED OF 0.15M/SEC BETWEEN THE SIMULATOR AND MOVEABLE PLATFORM (CONTAINING THE DOCKING MECHANISM). PROPER OPERATION OF THE DIFFERENTIAL IS VERIFIED DURING RING EXTENSION/RETRACTION AND OCCKING FOR A TEMPERATURE RANGE OF -50° C/-55°C TO 50°C/55°C.
- 5. CONTROLLED DOCKING TEST · CONTROLLED DOCKING IS PERFORMED UNDER LOAD CONDITIONS. A PULL TEST OF ASSEMBLIES WITH THE DOCKING MECHANISM ASSEMBLY IS PERFORMED DURING THIS TEST. THESE TESTS WILL VERIFY PROPER OPERATION OF THE DIFFERENTIAL.

DOCKING MECHANISM QUALIFICATION TESTS:

1. OPERATIONAL CAPABILITY TEST - DIFFERENTIAL MOVEMENT VERIFIED BY RING EXTENSION AND RETRACTION FROM THE END POSITION TO THE INITIAL POSITION THEN TO THE FORWARD POSITION AND FROM THE FORWARD POSITION TO THE END POSITION.



PAGE: 166 PRINT DATE: 08/25/96

# FAILURE MODES EFFECTS ANALYSIS (FMÉA) - CIL FAILURE MODE NUMBER: M4-1MR-8M010- 01

- 2. SHOCK AND SAWTOOTH LOADING STRENGTH TEST DOCKING MECHANISM IS SUBJECTED TO 20G TERMINAL SAWTOOTH SHOCK PULSES IN EACH AXIS, 3 PULSES IN EACH DIRECTION FOR A TOTAL OF 6 PULSES/AXIS, AFTER COMPLETION AN INSPECTION IS PERFORMED TO IDENTIFY BROKEN OR LOOSE HARDWARE AND AN OPERATIONAL CAPABILITY TEST IS CONDUCTED, AS DEFINED IN QTP #1 ABOVE, TO VERIFY PROPER DIFFERENTIAL OPERATIONS DURING RING MOVEMENT.
- 3. VIBRATION STRENGTH TEST APDS SUBJECTED TO THE FOLLOWING VIBRATION LEVELS IN EACH AXIS FOR A 400 SECOND DURATION.

FREQUENCY (HZ)	SPECTORAL DENSITY ACCELERATION
FROM 20 TO 90	INCREASING, 308 OCTAVE TO 0.067GZ/HZ
FROM BO TO 350	CONSTANT 0.087G2/HZ
FROM 350 TO 2000	DECREASING 3DB OCTAVE WITH 0.067QZ/HZ

SUBSEQUENT TO THIS TEST AN ENGINEERING INSPECTION IS PERFORMED TO IDENTIFY BROKEN OR LOOSE HARDWARE AND AN OPERATIONAL CAPABILITY TEST, AS DEFINED IN OTP #1 ABOVE, IS PERFORMED TO VERIFY PROPER DIFFERENTIAL OPERATIONS DURING RING MOVEMENT.

4. TRANSPORTABILITY STRENGTH TEST - SHIPPING LOADS ARE SIMULATED ON A VIBRATING TABLE TO VERIFY THAT THE DOCKING MECHANISM WILL NOT BE DAMAGED DURING SHIPMENT. THIS TEST IS CONDUCTED UNDER THE CONDITIONS CONTAINED IN THE FOLLOWING TABLE.

VIBRATION	VIBRATION		FREQUE	TOTAL TEST					
ACCELER	ACCELER	5-7	7-15	15-30	30-40	40-60	DURATION		
DIRECTION	AMPLITUDE		TEST	HP	MIN				
ALONG X-AX	S 1.4	<u> </u>	4	_		_	-	4	
1	1.2	76	93	32	<b>8</b> 1	38	5	7	
ALONG Y-AX	S 1.1	-	4		I— <del>-</del> -		-	4	
•	1.0	13	16	7	10	7	_	53	
ALONG Z-AXI	S 1.1	**	4			-	_	4	
	1.0	32	40	16	26	16	2	10	

SUBSEQUENT TO THIS TEST AN INSPECTION IS PERFORMED TO IDENTIFY BROKEN OR LOOSE HARDWARE AND AN OPERATIONAL CAPABILITY TEST, AS DEFINED IN QTP #1 ABOVE, IS PERFORMED TO VERIFY PROPER DIFFERENTIAL OPERATIONS DURING RING MOVEMENT.

5. APDS SERVICEABILITY TEST IN A SIX-DEGREE-OF-FREEDOM DYNAMIC TEST-THE SIX-DEGREE-OF-FREEDOM DYNAMIC TEST VERIFIES APDS DOCKING AND UNDOCKING OPERATIONS UNDER CLOSE-TO-FULL-SCALE CONDITIONS. STATIC MOTION OF ENTITIES IS SIMULATED UNDER SPECIFIC INERTIAL AND GEOMETRICAL PARAMETERS FOR VARIOUS INITIAL CONDITIONS FOR MIR/SHUTTLE DOCKING. A TOTAL OF 20 DOCKINGS IS PERFORMED. DIFFERENTIAL MOVEMENT VERIFIED BY EXTENSION OF DOCKING FING TO INITIAL POSITION AND ABSORPTION OF ENERGY OF RELATIVE MOVEMENT DURING EACH DOCKING WILL DETECT A JAMMED DIFFERENTIAL SUBSEQUENT TO THIS TEST AN ENGINEERING INSPECTION IS PERFORMED TO IDENTIFY BROKEN OR LOOSE HARDWARE AND AN OPERATIONAL CAPABILITY TEST, AS



PRINT DATE: 08/25/96

PAILURE MODES EFFECTS ANALYSIS (FMEA) — CIL FAILURE MODE, NUMBER: M8-1MR-BM010— 01

DEFINED IN OTP #1 ABOVE, IS PERFORMED TO VERIFY PROPER DIFFERENTIAL FUNCTIONING DURING RING MOVEMENT AND DOCKING OPERATIONS.

6. COLD AND HEAT RESISTANCE TEST - DOCKING OF THE MECHANISM IS THERMALLY CYCLED FROM +20°C TO -50/-55°C TO +50/+55°C TO +20°C IN A VACUUM AT 10°4 TO 10°5 TORR. DWELL AT EACH TEMPERATURE AND BETWEEN OPERATIONS AT EACH TEMPERATURE IS A MINIMUM OF 60 MINUTES AFTER STABILIZATION. FIVE CYCLES WERE PERFORMED AGAINST THE GUIDE RING EXTEND AND FINAL POSITION MECHANICAL STOPS FOR 10 SECONDS EACH. DURING EACH DOCKING, AS SHOWN IN THE FOLLOWING TABLE, A JAMMED DIFFERENTIAL WOULD BE DETECTED.

	DOCKING		ATOR AL ANGLE	TEMP	<b>VALUE</b>	PRESS INTEGRITY
SEQ	RATE,			<b>-</b>	VOLTAGE	
NO.	M/S	PITCH	ROLL	-c	VOLTS	CHECKOUT
· · · · · · · · · · · · · · · · · · ·	0.10	Ġ.	ဇ	25 +/-10	_23	YES
2	. 0.10	C*	4*	25 +/-10	34	NO
3	0.12	<b>4</b> °	4°	25 +/-10	27	NO
4*				+60+/-5		YES
4	0.10	<b>4</b> °	O°	+50+/-5	27	YES
5-		_	_	-(60+/-5)		YES
5	0.10	4°	0°	-(30+/-5)	27	YES_
6.			<del></del>	+60+/-5		YES
- 6	0.12	Do.	44	+50+/-5	_23	YES
ア				-( <del>60+/-5</del> )	_	YES
7	0.10	D.	4°	-(30 +/-5)	23	YES
8*				+60+/-5		YES_
8	0.12	4"	4*	50 +/-5	34	YES.
9-				-(60+√-5)	<del></del>	YES
9	0.12	4°	4*	-(30 +/-5)	34	YES
- 10*				+60+/-5		YES
10	0.10	4"	0"	+50+/-5	27	YES
11*		-		-{60+/-5}	_	YES_
11	0.10	O"	4"	-(30 +/-5)	27	YES
12*				+60+/-5		YES
12*	0.10	6	4"	+50+/-5	27	YES
13*		7 —		-(60+/-5)	·	YES
13"	0.12	. 4*	4*	-(30 +/-5)	27	YES
14*	<del>                                     </del>			+60+/-5		YES
14"	0.12	4	4*	+50+/-5	27	YES
15*	0.12	4-	4°	+25+/-10	23	YES

AFTER COMPLETION AN INSPECTION IS PERFORMED TO IDENTIFY BROKEN OR LOOSE HARDWARE AND AN OPERATIONAL CAPABILITY TEST, AS DEFINED IN QTP #1 ABOVE, IS PERFORMED TO VERIFY PROPER DIFFERENTIAL FUNCTIONING DURING RING MOVEMENT AND DOCKING OPERATIONS.



PAGE: 168 PRINT DATE: 08/25/96

# FAILURE MODES EFFECTS ANALYSIS (FMEA) — CIL FAILURE MODE NUMBER: MS-1MR-BM010-- 01

7. TARGET SERVICE LIFE TEST - TESTS ARE PERFORMED TO VERIFY PROPER DOCKING AND UNDOCKING OPERATIONS OVER ITS LIFE OF 100 DOCKINGS. PROPER OPERATION OF THE DIFFERENTIAL VERIFIED DURING 100 DOCKING AND UNMATING CYCLES (FOR MC621-0087-1001/-3001 UNITS ONLY). FOR MC621-0087-2001, -4001, & -5001 UNITS PROPER OPERATION VERIFIED DURING 388 CYCLES (44 VACUUM/LOAD CYCLES, 16 LOAD CYCLES, & 324 NO-LOAD CYCLES). THESE TESTS INCLUDE RING EXTENSION AND RETRACTION. SUBSEQUENT TO THIS TEST AN ENGINEERING INSPECTION IS PERFORMED TO IDENTIFY BROKEN OR LOGSE HARDWARE AND AN OPERATIONAL CAPABILITY TEST. AS DEFINED IN OTP #1 ABOVE, IS PERFORMED TO VERIFY PROPER DIFFERENTIAL FUNCTIONING DURING RING MOVEMENT AND DOCKING OPERATIONS.

- 8. BACKUP UNDOCKING MEANS CHECK PROPER OPERATION OF THE DIFFERENTIAL IS VERIFIED DURING COUPLING OF THE APDA ASSEMBLY WITH THE SIMULATOR.
- 9. CONTROL DISASSEMBLY UPON COMPLETION OF ALL QUAL TESTING THE DOCKING MECHANISM IS DISMANTLED AND ALL DIFFERENTIAL OPERATING SURFACES ARE CHECKED FOR EVIDENCE OF WEAR OR FAILURE.

OMRSD - TURNAROUND CHECKOUT TESTING IS ACCOMPLISHED IN ACCORDANCE WITH OMRSD.

## (C) INSPECTION:

RECEIVING INSPECTION
ALL COMPONENTS ARE SUBJECTED TO A 100% RECEIVING INSPECTION PRIOR TO INSTALLATION.

## CONTAMINATION CONTROL

CORROSION PROTECTION PROVISIONS AND CONTAMINATION CONTROL VERIFIED BY INSPECTION. CHECK OF ROOM CLEANLINESS; PARTS WASHING AND OTHER OPERATIONS OF THE TECHNOLOGICAL PROCESS WHICH PROVIDES CLEANLINESS ARE VERIFIED BY INSPECTION.

## CRITICAL PROCESSES

ANODIZING, HEAT TREATING, AND CHEMICAL PLATING VERIFIED BY INSPECTION.

## ASSEMBLY/INSTALLATION

TORQUE, ADJUSTMENTS AND TOLERANCES ACCORDING TO TECHNICAL REQUIREMENTS OF THE DRAWINGS ARE VERIFIED BY INSPECTION.

#### TESTING

ATP/QTP/OMRSD TESTING VERIFIED BY INSPECTION.

## HANDLING/PACKAGING

HANDLING/PACKAGING PROCEDURES AND REQUIREMENT FOR SHIPMENT VERIFIED BY INSPECTION.

## (b) FAILURE HISTORY:

DATA ON TEST FAILURES, UNEXPLAINED ANOMALIES, AND OTHER FAILURES EXPERIENCED DURING GROUND PROCESSING OF ODS DOCKING MECHANISMS CAN BE FOUND IN PRACA DATA BASE.



PRINT DATE: 29.08.95

| FAILURE MODES EFFECTS ANALYSIS (FMEA) - CIL FAILURE MODE

NUMBER: M8-1MR-BM010-- 01

(E) OPERATIONAL USE:

NONE FOR A COMPLETE JAMMING. HOWEVER AN INCREASE IN RESISTANCE CAN BE OVERCOME BY THE POWER OF THE DOCKING MECHANISM OR BY THE EXTERNAL FORCES OF DOCKING.

- APPROVALS -

DESIGN ENGINEER DESIGN MANAGER

NASA SS/MA

NASA SUBSYSTEM MANAGER

M. NIKOLAYEVA A. SOUSCHEV